

# (12) UK Patent Application (19) GB (11) 2 307 918 (13) A

(43) Date of A Publication 11.06.1997

(21) Application No 9624791.1

(22) Date of Filing 29.11.1996

(30) Priority Data

(31) 08567545 (32) 05.12.1995 (33) US

(71) Applicant(s)

Smith International Inc

(Incorporated in USA - Delaware)

PO Box 60068, 16740 Hardy Street, Houston,  
Texas 77205 - 0068, United States of America

(72) Inventor(s)

Zhigang Fang

(74) Agent and/or Address for Service

Saunders & Dolleymore  
9 Rickmansworth Road, WATFORD, Herts, WD1 7HE,  
United Kingdom

(51) INT CL<sup>6</sup>

B22F 5/00

(52) UK CL (Edition O )

C7D DB500 D812 D814 D830 D831  
E1F FFD

(56) Documents Cited

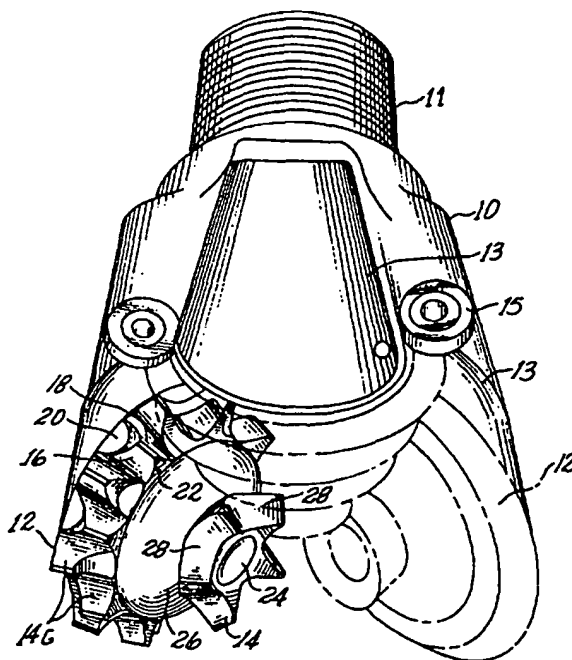
GB 2287959 A GB 1137053 A

(58) Field of Search

UK CL (Edition O ) C7D DB316 DB500  
INT CL<sup>6</sup> B22F 3/16 5/00  
Online W.P.I.

(54) Pressure molded powder metal milled tooth rock bit cone.

(57) A milled tooth shaped rotary cone drill bit for drilling oil wells and the like manufactured using a powder metallurgy process in which an alloy powder is pressure molded into the desired bit shape, sintered, and precision machined.

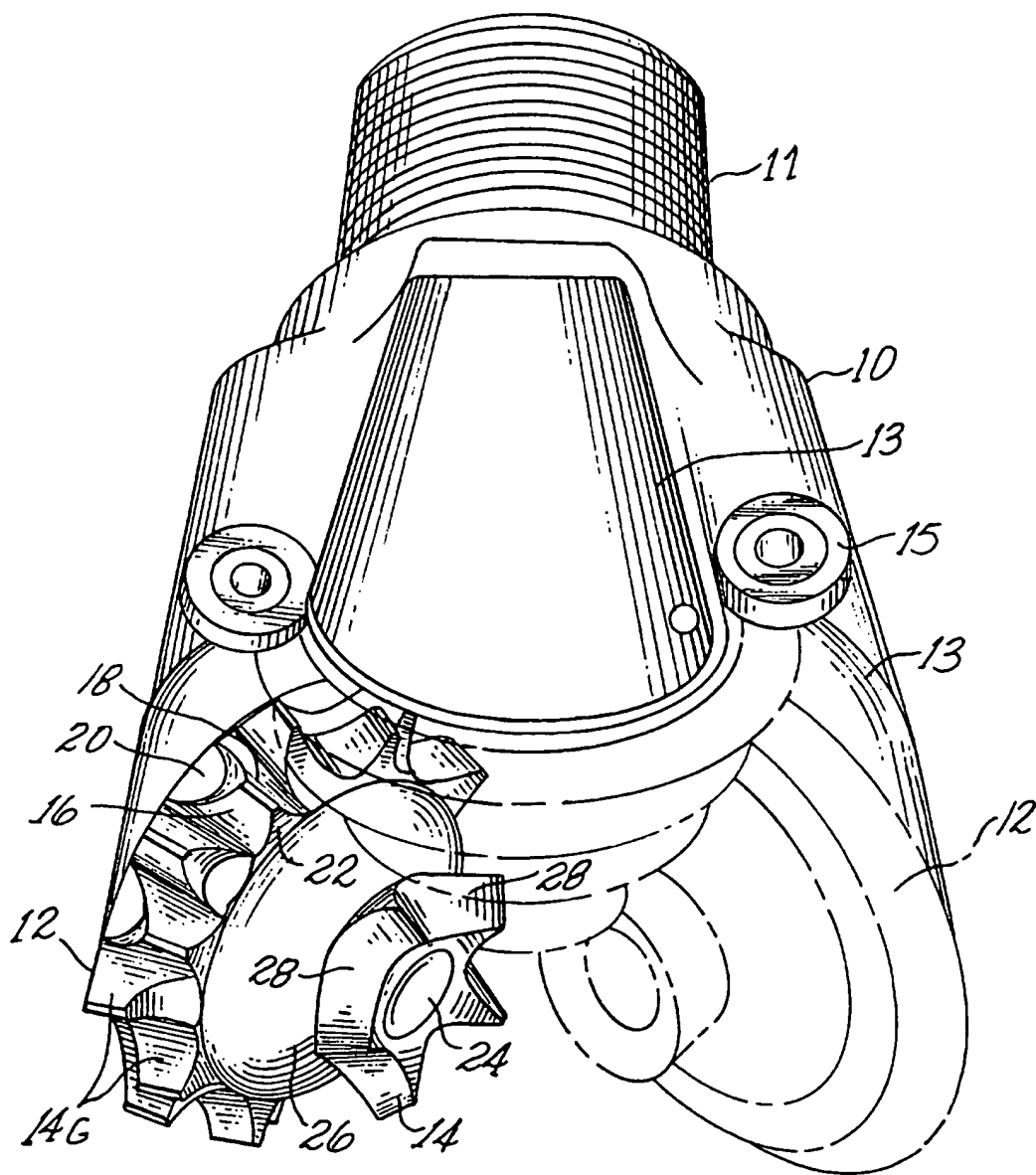


GB 2 307 918 A

At least one drawing originally filed was informal and the print reproduced here is taken from a later filed formal copy.

BEST AVAILABLE COPY

1/1



BEST AVAILABLE COPY

PRESSURE MOLDED POWDER METAL MILLED TOOTH ROCK BIT CONE

This invention relates to "milled" tooth rotary cone rock bits and methods of manufacture therefor.

Rotary cone rock bits for drilling oil wells and  
5 the like commonly have a steel body which is connected to  
the bottom of a long pipe which extends from the earth's  
surface down to the bottom of the well. The long pipe is  
commonly called a drill string. Steel cutter cones are  
mounted on the body for rotation and engagement with the  
10 bottom of the well being drilled to crush, gouge, and  
scrape rock thereby drilling the well. One important type  
of rock bit, referred to as a milled tooth bit, has  
roughly triangular teeth protruding from the surface of  
the cone for engaging the rock. The teeth are typically  
15 covered with a hard facing material harder than steel to  
increase the life of the cone. The teeth are formed into  
the steel cone by material-removal processes including  
turning, boring, and milling. Thus, the cone is referred  
to as a milled tooth rock bit cone because the teeth are  
20 manufactured by milling the teeth into a forged steel  
preform. The cones may also be referred to as steel tooth  
cones because they are predominantly manufactured from  
steel. A milled tooth rock bit cone can have 69 or more  
milled surfaces, five or more bores, and three or more  
25 turned surfaces. Thus, the production of a milled tooth  
rock bit cone is a labor intensive process, and a majority  
of the cost of a milled tooth rock bit cone is  
attributable to the labor cost. The cost is also  
increased by the waste of raw material which is machined  
30 away during the material removal process. The machining  
processes also leave sharp edges and corners on the  
finished cone. The sharp edges tend to crack, and the  
cracks propagate through the cone and through the hard  
facing, reducing the useful life of the cone. The sharp  
35 corners are plagued by stress concentrations which also

promote cracking of the cone. Thus, teeth geometry must be limited to avoid sharp edges and corners. Further, the geometry of the teeth is limited by the capability of the milling process making infeasible some tooth shapes that  
5 increase the rate of penetration without breakage.

To address these limitations, some powder metallurgy techniques have been suggested to manufacture "milled" tooth rock bit cones. For instance, one process currently used utilizes a pattern to form a flexible mold  
10 which is filled with powdered metal. The mold is cold isostatically pressed to partially densify the powdered metal. Isostatic pressure is pressure equally applied on all sides of the mold. The partially densified part, called a green part or preform, is then heated and rapidly  
15 compressed to full density by a quasi-isostatic process.

To create the preform, the powdered metal, usually steel, is poured into the flexible mold while the mold is vibrated. Vibrating the mold during filling uniformly packs the powder in the flexible mold. The  
20 flexible mold is supported during the cold isostatic pressing by tooling which allows the deformation necessary to compress the pattern. After the mold is compressed, the preform is removed from the mold and subjected to uniform heating. Once the preform is heated, it is  
25 transferred to a central position in a cylindrical compression cavity in which it is surrounded by a bed of granular pressure transfer medium heated to approximately the same temperature as the preform. The pressure transfer medium is then axially compressed creating a  
30 quasi-isostatic pressure field acting on all surfaces of the preform. The radial pressure acting on the preform approaches a theoretical maximum of one-half of the axial pressure acting on the preform. After compression, the part is removed from the cavity and allowed to cool slowly  
35 over a two (2) hour time period. This powder metallurgy

process requires two compression steps, and because the non-isostatic compression step causes a non-uniform reduction in size of the preform, its pattern is complex. The second compression process is essentially a hot pressing process, which is expensive and inefficient but only one part can be made at a time. Further, the steps required to prepare the part for the hot pressing process are complex and time consuming. Then, the process is not economical.

Other powder metallurgy process including powder injection molding have been utilized to fabricate small parts. In summary, this process begins by pelletizing or granulating a mix of powder metal and binder before injecting the pellets or granules into the mold. The mold is then removed, and the part is debinded and sintered. This process has only been utilized for small parts with thin cross-sections and heretofore has not been utilized for the production of milled tooth rock bit cones.

Thus, reduction in the required labor to fabricate a "milled" tooth rock bit cone is desirable to enhance the production rate and reduce production cost of the milled tooth rock bit cone. It is also desirable to diversify the geometric shapes of the teeth to increase the rate of penetration without the need for complexly shaped molds and preforms. Thus, the successful application of powder injection molding to produce "milled tooth rock bit cones" is desirable to bring about such an increase in the rate of penetration and decrease in the cost of rock bits which translates directly into reduction of drilling expense.

There is, therefore, provided in practice of this invention a novel method for manufacturing a toothed rotary cone rock drill bit. The method comprises the steps of pressure molding a blend of a binder with an alloy powder into a mold defining toothed rotary cone

shape thereby molding the blend into a toothed rotary cone shaped green part. In addition, the toothed rotary cone shape may contain an internal bearing surface which is machined to obtain the required tolerances for the bearing surface. Further, the blend may be subjected to pre-heating to facilitate filling the mold and to help the green part hold the desired shape until it is finally heated. In a preferred embodiment, the mold is made from water soluble material or other solvent soluble polymers. The mold is therefore consumable. To further increase the likelihood of the green part holding the desired shape until it is heated, the alloy powder may be pre-sintered.

In a preferred embodiment, the green part is subjected to a thermal debinding process in which the green part is slowly heated to 100°F and held at that temperature for one (1) hour. The green part is then heated to approximately 300°F and held at that temperature from eight (8) to ten (10) hours, and then the green part is heated to 400°F and held there for four (4) to eight (8) hours.

The invention is further directed to a toothed rotary cone rock drill bit manufactured by blending an alloy powder with a binder, pressure molding the alloy powder and the binder into the desired rock bit cone shaped green part, sintering/heating the green part, and machining the internal bearing surfaces. The rock bit cone is designed so that after sintering, the outer surface is the final net size, but the inner surface has extra material which allows precision machining of the inner surface to net size and shape.

These and other features and advantages of the present invention will be appreciated as the same becomes better understood by reference to the following detailed description when considered in connection with the accompanying drawing in which similar reference characters

denote similar elements and wherein:

FIG. 1 is a prospective view of a milled tooth rock bit cone formed by the powder metallurgy process of the present invention.

5           An exemplary milled tooth rock bit according to the present invention, shown in Fig. 1, comprises a stout steel body 10 having a threaded pin 11 at one end for connection to a conventional drill string (not shown). At the opposite end of the body, there are three rock bit  
10 cutter cones 12 for drilling rock for forming an oil well or the like. Each of the cutter cones is rotatably mounted on a pin (hidden) extending diagonally inward on one of the three legs 13 extending downwardly from the body of the rock bit. As the rock bit is rotated by the  
15 drill string to which it is attached, the cutter cones effectively roll on the bottom of the hole being drilled. The cones are shaped and mounted so that as they roll, teeth 14 on the cones gouge, chip, crush, break and/or erode at the rock at the bottom of the hole. The teeth  
20 14G in the row around the heel of the cone are referred to as the gage row teeth. They engage the bottom of the hole being drilled near its perimeter on "gage." Fluid nozzles 15 direct drilling mud into the hole to carry away the particles of rock created by the drilling.

25           Such a rock bit is conventional and merely typical of various arrangements that may be employed in a rock bit. For example, most rock bits are of the three cone variety illustrated. However, 1, 2, and 4 cone bits are also know. The arrangement of teeth on the cones is  
30 just one of many possible variations. In fact, it is typical that the teeth on the three cones in a rock bit differ from each other, so that different portions of the bottom of the hole are engaged by the three cutter cones; and collectively, the entire bottom of the hole is  
35 drilled. A broad variety of tooth and cone geometries

some of which are known can be fabricated utilizing the present invention, and these different tooth and cone geometries need not be further described for an understanding of the invention.

5               However, a short explanation of how the shape of the bit in Fig. 1 would be obtained using material removal processes is helpful. Each tooth would have four milled surfaces 16, 18, 20, and 22. The milled tooth rock bit cone would typically have three turned surfaces 24, 26,  
10              and the internal surface of the cone (not shown). Bores 28 would also be utilized in certain locations to aid in the material removal process. To avoid these labor intensive processes, powder metallurgy can be used to manufacture the cone.

15              Broadly, powder metallurgy is a class of processes whereby alloy powders comprising metals, ceramics, and other materials are molded into objects by compacting them in suitable dies and subsequently heating or sintering them at elevated temperatures to obtain the  
20              required density and strength. Alloy or metal powders are produced by many processes, including atomization, reduction, electrolytic deposition, thermal decomposition of carbonyl, mechanical comminution, precipitation from a chemical solution, production of fine chips by machining,  
25              and vapor condensation. Because the powders formed by the processes mentioned above have different sizes and shapes, it is necessary to blend them to obtain uniformity. During the blending phase, special physical and mechanical properties may be imparted to the toothed rotary rock bit  
30              cone by blending different metallic powders or other materials into the alloy powder. The blended alloy powder is then formed into the desired toothed rotary cone shape in dies or molds using hydraulically or mechanically actuated presses. The compaction obtains the required  
35              shape, density, and particle contact to impart sufficient



strength to the part to enable handling for further processing.

5       The preferred embodiment shown utilizes a steel powdered metal blended with a thermoplastic binder which is injection molded to form a green part having the desired cone geometry and larger than net size. The green part is then subjected to a debinding process at a temperature range between 100°F and 400°F inclusive. The green part is then sintered at temperatures from 800°C to 10       1300°C inclusive depending on the materials used to fabricate the cone. The outer surface including the teeth 14, is the final net shape after the sintering process. The internal surfaces of the rotary cone are designed to be near net shape after the sintering process.

15       Specifically, the internal bearing surfaces are designed to have extra material after the sintering process, so that the bearing surfaces can be precision machined to the proper dimensions. This is required because the bearing surfaces require low tolerances. The cone can be heat 20       treated to obtain the required ductility, hardness, and strength properties, and a hard facing material can be placed on the teeth. Though the preferred embodiment shown utilizing the present invention is a milled toothed shaped cone, the invention can easily be applied to 25       manufacture a bit or cone shaped to receive inserts.

      In detail, a preferred embodiment of the molding process includes pressure molding the blended alloy powder into a die or mold with an auger or press to obtain the necessary strength to enable further processing. The 30       pressure molding is conducted at less than approximately 100 psi. It is preferable to pull a vacuum in the mold before filling the mold with the powder metal. When a vacuum is pulled in the mold the pressure is approximately 1 atmosphere or 14.5 psi. To further increase the part's 35       ability to maintain its shape during processing, the

powder metal is blended with a thermal plastic binder before forming the powder into the desired shape. During pressure molding of a powder metal blended with a thermoplastic binder, the blend is heated to a temperature not high enough to melt the binder, but high enough to facilitate the flow of the blend into the mold. The temperature range is typically from 100°F to 150°F. Thus, the binder also acts as a lubricant during pressure molding to enable the blend to flow into the mold like a liquid, obtaining a more densified compact. The preferred plastic binder contains wax, kerosine, and a surfactant, usually duamine. The amount of plastic binder can be as great as fifty percent (50%) by volume. However, the usual range is from fifteen percent (15%) to forty percent (40%) by volume. Other binders include polyethylene and acetal resins. Water soluble materials such as polyvinyl alcohol can also be utilized as the binder.

The blend is then allowed to cool in the mold before the mold is removed. Preferably, the mold is a consumable, one-time use water soluble mold which dissolves in water. In a referred embodiment, the mold is made of polyvinyl alcohol, which is water soluble. For several reasons, the use of a consumable mold is advantageous over the use of a steel mold, which is used repeatedly. First rock bit designs change rapidly; so the useful life of the expensive steel mold is not fully utilized. Thus, the consumable mold allows greater versatility of rock bit designs, and further the complex rock bit slopes are more easily removed from consumable molds. The consumable mold is simply dissolved without placing any appreciable force on the part. With a steel mold, however, the multiple parts of the steel mold must be pulled apart. Pulling the mold pieces apart can put stress on the teeth or other protrusions of the part.

After removing or dissolving the consumable

mold, the cone produced by the molding process, commonly referred to as a green part, is thermally debinded. If the water soluble binder is used, the green part is debinded with water. Because of the large size of the cone and the thick cross sections of the cone, the thermal debinding process is more involved than for previous pressure molding processes. The green part is debinded from eight (8) to twentyfour (24) hours. Preferably, the green part is slowly heated to a first temperature of 100°F for one (1) hour. Then it is slowly heated to a second temperature of 300°F and held there for eight (8) to ten (10) hours, and then it is heated further to a third temperature of 400°F and held there for another four (4) to eight (8) hours.

After debinding, both the inner and outer surfaces of the cone are larger than net size. To bring the cone to full density and net size, the green part is subjected to heat in a controlled atmosphere furnace at a temperature typically just below the melting point of the alloy powder and sufficiently high to allow the bonding of the individual particles. This process, referred to as sintering, is performed at a temperature range of 800°C to 1300°C depending on the materials used in the cone. Because the green part is quite weak and has a low strength, the green part may be pre-sintered by heating it to a temperature lower than the normal temperature for final sintering.

Sintering can be conducted in the solid phase, liquid phase, or supersolidus liquid phase, depending on alloys used. When liquid phase sintering is used with steel powder, the powder metal is alloyed with copper or boron. Both boron and copper create a liquid between solid iron molecules at lower temperatures, but the copper results in actual liquid phase sintering. Copper and its alloys can also be used in an infiltration process to

eliminate porosity in the cone. Further, a conventional hot isostatic pressing step might be necessary to achieve 100% density for some alloys.

5 After sintering, the outer surface of the cone is net size and shape, but parts of the inner surface of the cone have excess material that is machined away to create the internal bearing surfaces. Additional processes, such as heat treating and hard facing, can be performed on the cone as required by the intended use for  
10 the cone.

Utilizing the present invention, significant machining costs are avoided, and the configuration of the teeth is no longer limited by the capability of material removal operations. Sharp edges and corners are largely  
15 eliminated, and tooth shapes impossible to obtain through material removal processes can be obtained with powder metallurgy. Rock bit cones manufactured according to the present invention can utilize tooth configurations which increase the rate of penetration and tooth shapes which  
20 facilitate hard facing of the teeth, thereby increasing the life of the cone. Further, there is a reduction in the use of raw materials because far less of the original cone is machined away.

Thus, a toothed rotary cone rock drill bit is  
25 disclosed which utilizes pressure molding to more efficiently obtain the desired bit designs and to create bit designs which were before infeasible. While embodiments and applications of this invention have been shown and described, it would be apparent to those skilled  
30 in the art that many more modifications are possible without departing from the inventive concepts herein. It is, therefore, to be understood that within the scope of the appended claims, this invention may be practiced otherwise than as specifically described.

CLAIMS

1. A method of manufacturing a toothed rotary rock bit cone comprising:  
pressure molding a blend of an alloy powder and  
5 a binder into a mold to form a toothed rotary cone shaped green part having a plurality of teeth; and  
heating the green part.
2. The method of Claim 1 further comprising:  
preparing an alloy powder;  
10 blending the alloy powder with a binder; and  
pelletizing the blend.
3. The method of claim 1 wherein the mold is consumable, and further comprising removing the green part from the mold.
- 15 4. The method of Claim 3, wherein the consumable mold is dissolved.
5. The method of claim 1 wherein the pressure molding is performed at less than approximately 100 psi.
6. The method of Claim 1, further comprising  
20 pulling a vacuum in the mold.
7. The method of Claim 6, wherein the pressure molding is performed at approximately one atmosphere of pressure.
8. The method of Claim 1, further comprising  
25 debinding the green part.
9. The method of Claim 8, wherein the green part is debinded with water.
10. The method of Claim 1, wherein the mold comprises a consumable mold.
- 30 11. The method of Claim 8, where in the green part is thermally debinded.
12. The method of Claim 11, wherein the thermal debinding comprises:  
slowly raising the temperature of the green  
35 part to a first temperature, and holding it at the first temperature for a first period of time;  
slowly raising the temperature of the green part to a second temperature, and holding it at the second

temperature for a second period of time; and

slowly raising the temperature of the green part to a third temperature and holding it at the third temperature for a third period of time.

5 13. The method of Claim 12, wherein the first temperature is approximately 100°F, the second temperature is approximately 300°F, and the third temperature is approximately 400°F.

10 14. The method of Claim 12, wherein the first time period is approximately 1 hour, the second time period is from approximately 8 hours to approximately 10 hours, and the third time period is from approximately 4 hours to approximately 8 hours.

15 15. The method of Claim 1, further comprising:  
pressure molding the blend into a toothed rotary cone shape having at least one internal bearing surface; and machining at least one internal bearing surface.

20 16. The method of Claim 1, further comprising heat treating the green part after heating.

17. The method of Claim 1, further comprising bonding a hard facing material onto the teeth.

18. The method of Claim 1, wherein the alloy powder is a steel powder.

25 19. The method of Claim 1, wherein the binder is a thermal plastic binder.

20. The method of Claim 1, further comprising heating the blend to between approximately 100 F and approximately 150°F.

30 21. The method of Claim 1, further comprising the step of pre-sintering the alloy powder.

22. A method of manufacturing a toothed rotary cone rock bit comprising the steps of:

35 fabricating a mold defining a toothed rotary cone shape having a plurality of teeth and at least one internal bearing surface;

preparing an alloy powder;

blending the alloy powder with a binder;

pressure molding the alloy powder and the binder into the mold to form a toothed rotary cone shaped green part;

removing the green part from the mold;

5 thermally debinding the green part for at least 12 hours at temperature range from approximately 100°F to approximately 400°F;

sintering the alloy powder; and

machining the internal bearing surface.

10 23. The method of Claim 22, further comprising heating the blend of the alloy powder and binder before pressure molding.

24. A toothed rotary cone rock drill bit comprising a body including a plurality of teeth and at least one  
15 internal bearing surface, the body being formed by preparing an alloy powder, blending the alloy powder with a binder, pressure molding the alloy powder and the binder into a mold, sintering the blend and machining the bearing surface.

20 25. The bit of Claim 24, wherein the body is further formed by pre-sintering the alloy powder.

26. The bit of Claim 24, wherein the green part comprises an outer surface and an inner surface and the green part is formed by molding the outer surface and the  
25 inner surface to larger than net size, sintering the green part such that the outer surface is net size and the inner surface is at least in part larger than net size, and machining at least part of the inner surface to net size.

27. The bit of Claim 25, wherein the body is further  
30 formed by heating the blend of alloy powder and binder.



Application No: GB 9624791.1  
Claims searched: 1-26

Examiner: R.B.Luck  
Date of search: 29 January 1997

**Patents Act 1977**  
**Search Report under Section 17**

**Databases searched:**

UK Patent Office collections, including GB, EP, WO & US patent specifications, in:

UK CI (Ed.O): C7D DB316,DB500

Int CI (Ed.6): B22F 3/16,5/00

Other: Online W.P.I.

**Documents considered to be relevant:**

Category	Identity of document and relevant passage	Relevant to claims
A	GB2287959 Baker Hughes Inc.	1
A	GB1137053 SHELL	1

X Document indicating lack of novelty or inventive step  
Y Document indicating lack of inventive step if combined with one or more other documents of same category.  
& Member of the same patent family

A Document indicating technological background and/or state of the art.  
P Document published on or after the declared priority date but before the filing date of this invention.  
E Patent document published on or after, but with priority date earlier than, the filing date of this application.